#### General Properties of Detectors

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- 3. Geometry effects
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# Section 1

# Introduction

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#### 1. Introduction

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# Detector model (simplified)

- Before discussing different types of detectors let's study some general properties that apply to all of them.
- Let's consider a simplified view of a detector system:



S = # part/s emmitted by the source

r = # part/s recorded by the system

 $r = f_1 f_2 f_3 \cdots f_n S$ 

• The *f*'s are represent the effects of the setup on the measurement:

- Geometry effects
- Source effects
- Detector effects
- As important as these effects is the way the detector is operated.

#### Absolute and relative measurements

- An absolute measurement is one in which the exact number of particles emitted or the exact numbers of events taking place is determined:
  - Determination of the activity of a source
  - Measurement of a cross section
- In a relative measurement, we are not interested in the exact number of events or particles emitted. A fraction of these is measured.
  - The presence or not of a certain type of radiation
  - Variation of flux of particles
- In case of relative measurement there is a relationship with the absolute measurement, but it's not necessary to know it.
- In general, relative measurements are easier than absolute measurements.
  - In absolute measurements we need to know ALL f factors
  - In relative measurements don't.

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# Section 2

# Modes of detector operation

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#### 2. Modes of detector operation

Introduction Signal Generation Pulse mode Current mode Mean Square Voltage mode

# Modes of detector operation

- Net result of radiation interaction with matter is the appearance of a given amount of charge *Q*:
  - Charge collection thanks to electric field between electrodes
  - It appears current in the electrodes
  - Collection time depends on each detector



• We are going to study three modes of detector operation

- > Pulse mode: designed to record each individual quantum of radiation
- Current mode: current average taken over many events
- Mean Square voltage: average sensitive to  $Q^2$

# Signal Generation

- Signals from detectors arise because of the motion of charge carriers after they are formed by incident radiation
  - Induced charge in electrodes due to moving charges
  - Signal induced is created as soon as charge carrier starts to move
- General method to calculate induced charge on electrodes

$$i(t) = q \vec{v} \cdot \vec{E}_w \longrightarrow$$
 Shockley-Ramo theorem

- q : is the charge of the charge carrier
- $\vec{v}$  : velocity of charge carrier.  $\vec{v} = \mu \vec{E}$

$$\vec{E} = -\nabla \phi$$

 $\vec{E}_w$  : Weighting field. How moving particles couples to the electrode

$$\vec{E}_w = -\nabla \phi_w$$

• The induced charge on the electrode by a charge carrier is given by:  $\label{eq:Q} Q = q \Delta \phi_0$ 

 $\Delta \phi_0$ : Difference in weighting potential from beginning to the end of carrier path

# Weighting field

- Knowing  $\phi$  and  $\phi_w$  we can know/simulate induced charge in electrodes
- To compute  $\phi$  we need to solve the Poisson equation

$$\nabla^2 \phi = \frac{\rho}{\epsilon}$$

with all contour conditions imposed by the detector.

- To compute the weighting field of an electrode we have to:
  - Set to 1 V the voltage of the electrode for which we can calculate the induced current
  - Set to 0 V the rest of the voltages
  - Any trapped charge is ignored in the calculation.

$$\nabla^2 \phi_w = 0$$

- Best method to calculate  $\phi$  and  $\phi_w \rightarrow$  Finite element methods
- Simple cases can be calculated analytically.

#### Pulse mode

- In this mode we want to keep track of individual radiation events
- We will have access to the amplitude and time information.
- Signal pulse will depend on the input circuit connected to the detector

- Preamplifier (see Electronics chapter) = net of resistors/capacitors
  - R=Input Resistance of the circuit
  - C=Total capacitance (circuit+detector)
  - Basic parameter  $\tau = RC$
  - Signal obtained V(t) along R

# Pulse mode

•  $RC \ll t_c$ :

 $i_R(t)\simeq i(t) \to v_R(t)=i(t)R$ 

- This is the configuration if we want to access to timing info.
- Time-of-flight
- High-rate scintillators
- $RC >> t_c$ :
  - $t < t_c$ : charge integration in C
  - $t > t_c$ : C discharge through C
  - Leading edge depends on detector (t<sub>c</sub>)
  - Trailing edge depends on the circuitry
  - $V_{max} = \frac{Q}{C} \propto$  charge deposited
  - Info about energy deposited, particle type,etc
  - Requires use of a CSA



# Current mode

- The measuring circuitry has a fixed response time  $T >> t_c$
- It averages the current over this time T



• Suitable for high fluxes where pulse mode cannot be applied

► Radioprotection → Immediate control if ionization

### Current mode

• In case of steady radiation we can calculate  $I_0$  and  $\sigma_i(t)$ 

 $I_0 = rQ = r\frac{E}{w}q \quad \rightarrow$ 

Q = charge produced for each event E = average energy deposited per event w = average energy to produce an ion pair q =  $1.6 \times 10^{-19} C$ 

- ... and the standard deviation  $\sigma_i(t)$ 
  - From Poisson statistics, the  $\sigma$  over the number of events is

$$n = rT \quad \Rightarrow \quad \sigma_n = \sqrt{n} = \sqrt{rT}$$

r = event rate

► If all events leave in average same charge Q

$$\frac{\sigma_i(t)}{I_0} = \frac{\sigma_n}{n} = \frac{1}{\sqrt{rT}} \qquad \rightarrow \qquad \overline{\sigma_i(t)} = \frac{I_0}{\sqrt{rT}}$$

# Mean Square Voltage Mode

- Statistical properties of the signal in current mode allow this mode
- Signal is sent through an element that blocks the DC part of  $I_0$ , and allow only pass the fluctuation  $\sigma_i(t)$
- Additional signal processing can square this signal and average it



- Signal is proportional to mean charge Q produced in each event
- Enhanced events where Q is large
  - Useful in case of mix radiation
  - > In a nuclear reactor, neutron signal will be larger than photon signal

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# Section 3 Geometry effects

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#### 3. Geometry effects

Effect of the Medium Solid Angle

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#### Geometry effects

- Geometry effects take into account factors as the size and shape of both source and detectors as well as the distance between them
- The geometry can affect to the measurement in two ways:
  - The influence of the medium between the source and the detector
  - The exact size and shape of the source and the detector as well as the distance between them. This a purely geometrical effect that it will be taken into account with the solid angle.



# Effect of the Medium

- Let's consider a source and a detector separated a distance d.
- In most of the cases, the medium is either air or other low density medium
- The effect of the medium depend on various factors
  - The medium: both Z and its density.
    Differential cross sections depends on Z
    Macroscopic cross sections depend of ρ
  - The type of particle.
    Different energy loss behaviors for charged and neutral particles.
    Absorption and scattering processes.
    Buildup effects.
- Important effect that should be taken into account specially when dealing with low energy or low intensity phenomena.
- Influence of the medium can always be avoided performing the measurement in vacuum, at the price of increase the complexity of the setup.

# Solid Angle: Intuitive definition

- The concept of solid angle will allow us to determine the fraction of particles emitted by the source that will enter into the detector
- For an intuitive definition, let's consider an isotropic point source.
- Since particles are emitted with equal probability in all directions, only a fraction of them will reach the detector.



- This fraction of particles is equal to the solid angle  $(\Omega)$  subtended by the detector.
- In a general case of an extended source we can apply also this definition.

 $\Omega = \frac{\# \text{ particles emitted inside the aperture of the detector}}{2}$ 

# particles emitted by the source

# Solid Angle

- To derive the mathematical expression, let's consider the following:
  - A plane source of area A<sub>s</sub> emitting S<sub>0</sub> particles/(m<sup>2</sup> s) isotropically
  - A detector of area  $A_d$  at a distance d
  - Let's consider two differential areas dA<sub>s</sub> and dA<sub>d</sub> and integrating

$$\Omega = \frac{\int_{A_s} \int_{A_d} \left( S_0 \frac{dA_s}{4\pi r^2} \right) dA_d(\hat{n} \cdot \hat{r})}{S_0 A_s}$$
$$\downarrow \quad \hat{n} \cdot \hat{r} = \cos w$$
$$\Omega = \frac{1}{4\pi A_s} \int_{A_s} dA_s \int_{A_d} dA_d \frac{\cos w}{r^2}$$



- This equation is valid for any shape of source and detector
- $\Omega$  is the fractional solid angle  $(0 \le \Omega \le 1)$

• Point Isotropic Source and a Detector with a Circular Aperture



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• Disk Source Parallel to a Detector with a Circular Aperture



• Point Source and a Detector with a Rectangular Aperture



$$\Omega = \frac{1}{4\pi} \arctan \frac{ab}{d\sqrt{a^2 + b^2 + d^2}}$$

• If the source is located at an arbitrary point above the detector, the solid angle is the sum of four terms.

$$\Omega = \Omega_1 + \Omega_2 + \Omega_3 + \Omega_4$$

• Disk Source and a Detector with a Rectangular Aperture



• Disk Source and a Detector with a Rectangular Aperture

$$\begin{split} \Omega &= \frac{w_1 w_2}{4\pi} \left[ 1 + \frac{3}{4} \phi^2 - \frac{1}{2} (w_1^2 + w_2)^2 + \frac{1}{8} (5\phi^4 + 3w_1^4 + 3w_2^4) \right. \\ &+ \frac{5}{4} \phi^2 (w_1 + w_2) - \frac{35}{64} \phi^6 + \frac{5}{12} w_1^2 w_2^2 - \frac{35}{16} \phi^4 (w_1^2 + w_2^2) \right. \\ &- \frac{7}{32} \phi^2 (9w_1^4 + 9w_2^4 + 10w_1^2 w_2^2) - \frac{7}{16} w_1^2 w_2^2 (w_1^2 + w_2^2) \\ &- \frac{5}{16} (w_1^6 + w_2^6) \right] \end{split}$$

 $w_1 = a/d$   $w_2 = b/d$   $\phi = R_s/d$ 

• If the source is located at an arbitrary point above the detector, the solid angle is the sum of four terms.

# Solid Angle calculation by Monte Carlo methods

- The basic equation of the solid angle can be solved analytically in very few simple and symmetric cases
- In some other cases, approximate solutions can be obtained by series expansions or numerical integration
- The most general method that can be used with any geometry is based on Monte Carlo calculation
  - Easy source-detector geometry definition
  - Initial particle position and angle determined from random numbers
  - Track particle to see if intersects detector volume
  - Solid angle defined as

$$\Omega = \frac{\text{\# particles hitting detector}}{\text{\# particles generated}}$$

• Error decreases with increasing number of generated particle.

# Solid angle = Geometric efficiency

- Be careful:
  - The same detector and source may have different solid angles depending on the experimental setup.
  - The geometric efficiency is NOT an intrinsic characteristic of a detector.
  - It takes into account the relative position between the detector and the radiation source



# Section 4

# Source effects

General Properties of Detectors

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#### 4. Source effects

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#### Source effects

- Radioactive deposit
  - Self Absorption factor
  - Backscattering factor

- Beams
  - Size
  - Intensity
  - In-beam interaction

# Section 5

# Detector effects

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#### 5. Detector effects

Efficiency Energy resolution. Fano Factor Dead Time

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#### Detector effects

- The detector itself may affect the measurement in various ways.
  - Through its walls and entrance windows
  - Its intrinsic detection efficiency
  - Different detectors can react differently to the same radiation
  - The recovery time (if any) after a particle is detected
  - The readout mode



# Efficiency

- One of the main characteristics of a detector system
- It accounts the number of events registered by a detector wrt certain numbers of events.
  - ► Both terms numerator and denominator should always be well defined
  - ► It depends on: radiation type, rate, detector, readout, geometry, ...

Intrinsic	$\varepsilon_{int} = \frac{\# \text{ events registered}}{\# \text{ events impinging the detector}}$
	$\varepsilon_{int} = 1 - e^{-\mu x}$
Absolute	$\varepsilon_{abs} = \frac{\# \text{ events registered}}{\# \text{ events emitted by source}}$
Relative	$\varepsilon_{rel} = \frac{\# \text{ events registered by det } 1}{\# \text{ events registered by det } 2} = \frac{\varepsilon_{int,1}}{\varepsilon_{int,2}}$
Peak	$\varepsilon_{peak} = \frac{\# \text{ events registered in a peak}}{\# \text{ events impinging the detector}}$

- BE CAREFUL: It's a relative measurement
- Definitions are related:

$$\varepsilon_{abs} = \varepsilon_{int} \Omega$$

# Energy resolution

- This characteristics is applicable only if we measure the energy.
- It measures the ratio of the FWHM of an energy peak with the mean of this peak

$$R = \frac{\Delta E}{E}$$
$$R_1 = \frac{\mathsf{FWHM}_1}{E_0} < \frac{\mathsf{FWHM}_2}{E_0} = R_2$$

FWHM =  $2.35\sigma$  if gaussian distribution

• Cuased by:

- drifts of detector properties
- random noise
- statistical noise



N = E/w: Number ions pairs generated

# Energy resolution: Statistical approach

• Calculation of R as a function of N is based on Poisson statistics:



#### Fano Factor

- The expression  $R = \frac{2.35}{\sqrt{N}}$  is indeed an upper limit of the energy resolution.
  - Experience shows that some detectors can achieve energy resolution smaller than the one predicted
  - The reason of this behavior is that the processes generating the charge carriers are not independent.
- Fano factor has been introduced to take into account this deviation.

$$F = \frac{\text{observed variance in } N}{\text{Poisson variance in } N} = \frac{\sigma_{obs}^2}{\sigma_{Poisson}^2} \qquad \begin{array}{l} \text{Scintillators} \\ \text{Semiconductors} \\ \text{Prop. Counters} \end{array} \qquad \begin{array}{l} F = 1 \\ F \sim 0.083 - 0.143 \\ F \sim 0.12 \end{array}$$
$$\sigma_{obs}^2 = F \sigma^{Poisson} \end{array}$$

### Fano Factor

$$F = \frac{\text{observed variance in } N}{\text{Poisson variance in } N} = \frac{\sigma_{obs}^2}{\sigma_{Poisson}^2}$$

Scintillators	F = 1
Semiconductors	F ~ 0.083-0.143
Prop. Counters	$F \sim 0.12$

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$$\sigma_{obs} = \sqrt{F} \sigma_{Poisson}$$

$$R_{Poisson} = \frac{2.35}{\sqrt{N}}$$
$$R_{stat} = \frac{2.35\sigma_{obs}}{N} = \frac{2.35\sqrt{F}\sigma_{Poisson}}{N} = 2.35\sqrt{\frac{F}{N}}$$

• In case other sources of uncertainty they will add quadratically

$$FWHM_{total}^2 = FWHM_{stat}^2 + FWHM_{noise}^2 + FWHM_{drift}^2 + \cdots$$

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Why is the energy resolution for a Ge-detector much better than for a scintillator?



 $R = 2.35 \sqrt{\frac{Fw}{E}}$  Scintillators:  $R \sim 5 - 10\%$  w = 30 - 100 eV  $F \sim 1$ Germanium: R < 1% w = 2 - 3 eV  $F \sim 0.1$ 

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# Dead Time

- It's the finite time required by a detector system to process an event
- During this time the detector is insensitive.
- Any event arriving to the detector during this time will not be detected.



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# Dead Time: Causes and Types

- Major causes of dead time:
  - Detector itself: i.e. electrical discharge in a GM ~400  $\mu$ s to recover
  - Readout electronics: Gate generation
  - Logic: Vetos from external systems
- We can distinguish two types of dead time behaviour:
  - Paralyzable or extendable
  - Non-Paralyzable



#### Dead Time: Non-paralyzable case

- Let's consider n = true interaction rate m = recorded count rate  $\tau =$  system dead time
- Non-paralyzable case:
  - Fraction of time the detector is "dead" =  $m\tau$
  - Rate at which event are lost =  $nm\tau$

$$n = m + nm\tau \quad \rightarrow \quad n = \frac{m}{1 - m\tau}$$

#### Dead Time

# Dead Time: Paralyzable case

- Paralyzable case:
  - Dead time periods are not of fixed length
  - m = rate of occurrences of time intervals between true events larger than  $\tau$
  - Distribution on intervals between random events is:

$$P_1(t)dt = ne^{-nt}dt$$

 $P_1(t)dt$  = distribution of intervals between random events occurring at an average rate n

• Probability of intervals larger than  $\tau$ 

$$P_2(\tau) = \int_{\tau}^{\infty} P_1(t) dt = e^{-nt}$$

Rate of occurrence of such intervals:

$$m = ne^{-n\tau}$$

#### Dead Time: Paralyzable vs Non-Paralyable



### Dead Time: Two sources method

- Based on counting rates of two sources individually and in combination.
  - $n_1, n_2, n_{12}, n_b$  true counting rates
  - $m_1, m_2, m_{12}, m_b$  observed rates

$$n_{12} - n_b = (n_1 - n_b) + (n_2 - n_b)$$

$$n_{12} + n_b = n_1 + n_2$$

• Assumed non-paralyzable model  $n = \frac{m}{1-m\tau}$ 

$$\frac{m_{12}}{1 - m_{12}\tau} + \frac{m_b}{1 - m_b\tau} = \frac{m_1}{1 - m_1\tau} + \frac{m_2}{1 - m_2\tau}$$

• Solving this equation gives

$$\tau = \frac{X(1 - \sqrt{1 - Z})}{Y} \qquad \qquad \begin{array}{l} X = m_1 m_2 - m_b m_{12} \\ Y = m_1 m_2 (m_{12} + m_b) - m_b m_{12} (m_1 + m_2) \\ Z = \frac{Y(m_1 + m_2 - m_{12} - m_b)}{X^2} \end{array}$$

# Dead Time: Decaying source method

- Measure the departure of observed counting rate from a the known exponential decay of a short lived radioisotope:  $n = n_0 e^{-\lambda t} + n_h$
- In the limit of negligible background  $n \simeq n_0 e^{-\lambda t}$



# Section 6

# Detector Response Function

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6. Detector Response Function

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# Pulse Height Spectra

- When operating the detector in pulse mode we have access to energy distribution
- We define the response function for an energy *E* as the spectrum of pulse heights observed from the detector when it's reached by a mono-energetic radiation

$$PH(E) = \int S(E')R(E,E')dE'$$

- ► S(E') = Spectrum of incident particles
- R(E, E') = Response function



# Counting Curves and Plateau

- In pulse mode, events fed a counting system if pulse heights  $> H_t$
- Operating mode (Gain + threshold) should be determined to assure stability of the measurements



# Counting Curves and Plateau

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